

Coating of Automobile Structural Components from Ultra-High Strength Steels

5th International Conference on Sustainable Automotive Technologies 25.-27.09.2013

V. Merklinger, B. Wielage, T. Lampke, S. Steinhäuser, TU Chemnitz
B. Reinhold, Audi AG; C. Strobl, TH Ingolstadt



Content

1

Corrosion Protection of Ultra-High Strength Steels

2

Alloy Development: Zn-Al-Mg System

3

Microstructure Characterization

4

Corrosion Performance

5

Summary

Corrosion Protection of Ultra-High Strength Steels

1

Corrosion Protection of Ultra-High Strength Steels

2

Alloy Development: Zn-Al-Mg System

3

Microstructure Characterization

4

Corrosion Performance

5

Summary

Motivation, Goal of the Project

Motivation

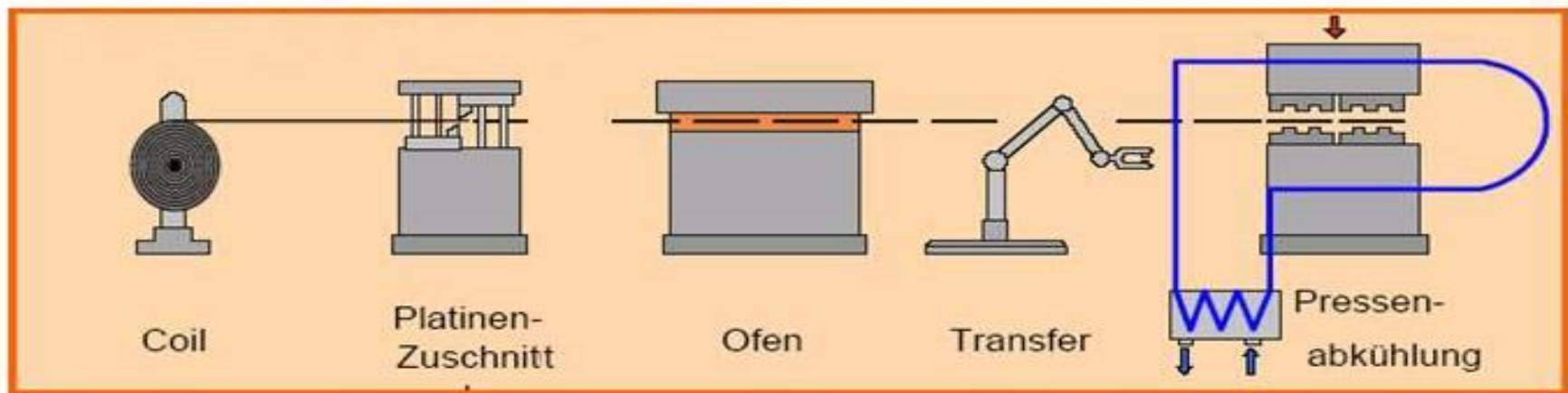
- Increasing lightweight applications of hot-stamped steel in automotive structure parts
- Due to manufacturing process no suitable corrosion protection of parts available
- Established corrosion protection for steel with Zn-Al or Zn-Mg alloys
- Increased corrosion protection with Zn-Al-Mg vgl. ZAM®

Goal of the project

- Development of a new corrosion protection system based on hot dip galvanizing in the Zn-Al-Mg system for high-strength steels without annealing effects for substrate

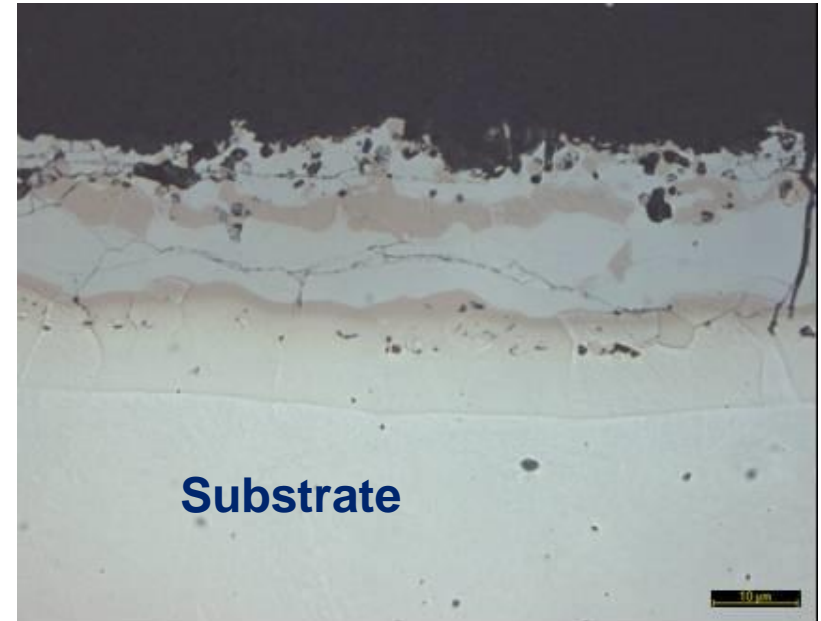
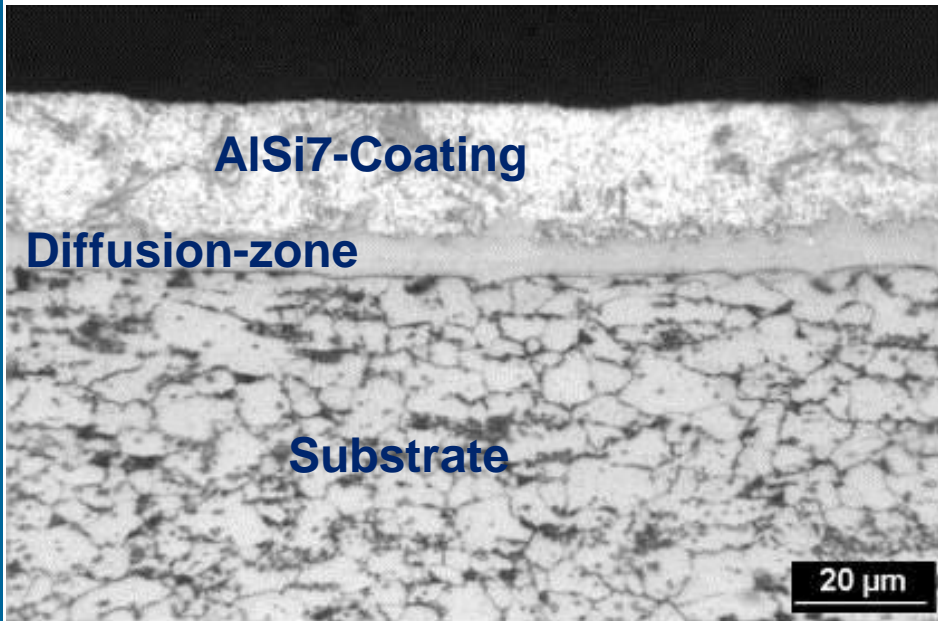
Process Description – In-Mould Hardening

- Austenitisation in furnace 9 min, 950 °C
- Die quenching with a cooling rate of 50 K/s
- Transformation to final parts with martensitic microstructure



Problem: Which coating survives this treatment?

State of the Art



Usibor 1500 P – original structure

Usibor 1500 P - hardened

Corrosion Protection of High-Strength Steels

Alloy Development Zn-Al-Mg System

1

Corrosion Protection of Ultra-High Strength Steels

2

Alloy Development: Zn-Al-Mg System

3

Microstructure Characterization

4

Corrosion Performance

5

Summary

Problem

Problem:

Decreasing tensile strength due to heat treatment

- Original state: R_m 1800 MPa $\epsilon_{\text{Bruch}} \sim 4,5 \%$
 - 350 °C R_m 1250 - 1350 MPa $\epsilon_{\text{Bruch}} 2,7 - 3,5 \%$
 - 375 °C R_m 1280 - 1320 MPa $\epsilon_{\text{Bruch}} 2,7 - 3,2 \%$
 - 400 °C R_m 1200 - 1300 MPa $\epsilon_{\text{Bruch}} 2,7 - 3,0 \%$
 - 620 °C R_m 850 - 900 MPa $\epsilon_{\text{Bruch}} 6,5 - 7,5 \%$
- Best dip temperature: 350 to 390 °C

Solution

Low Temperature Galvanizing

Solution LTG:

Low Temperature Galvanizing

- Melting process
- Hot dip galvanising
- Reduction of melting point temperature by eutectic alloy

Alloy Development

Phase Diagram Zinc-Aluminium-Magnesium

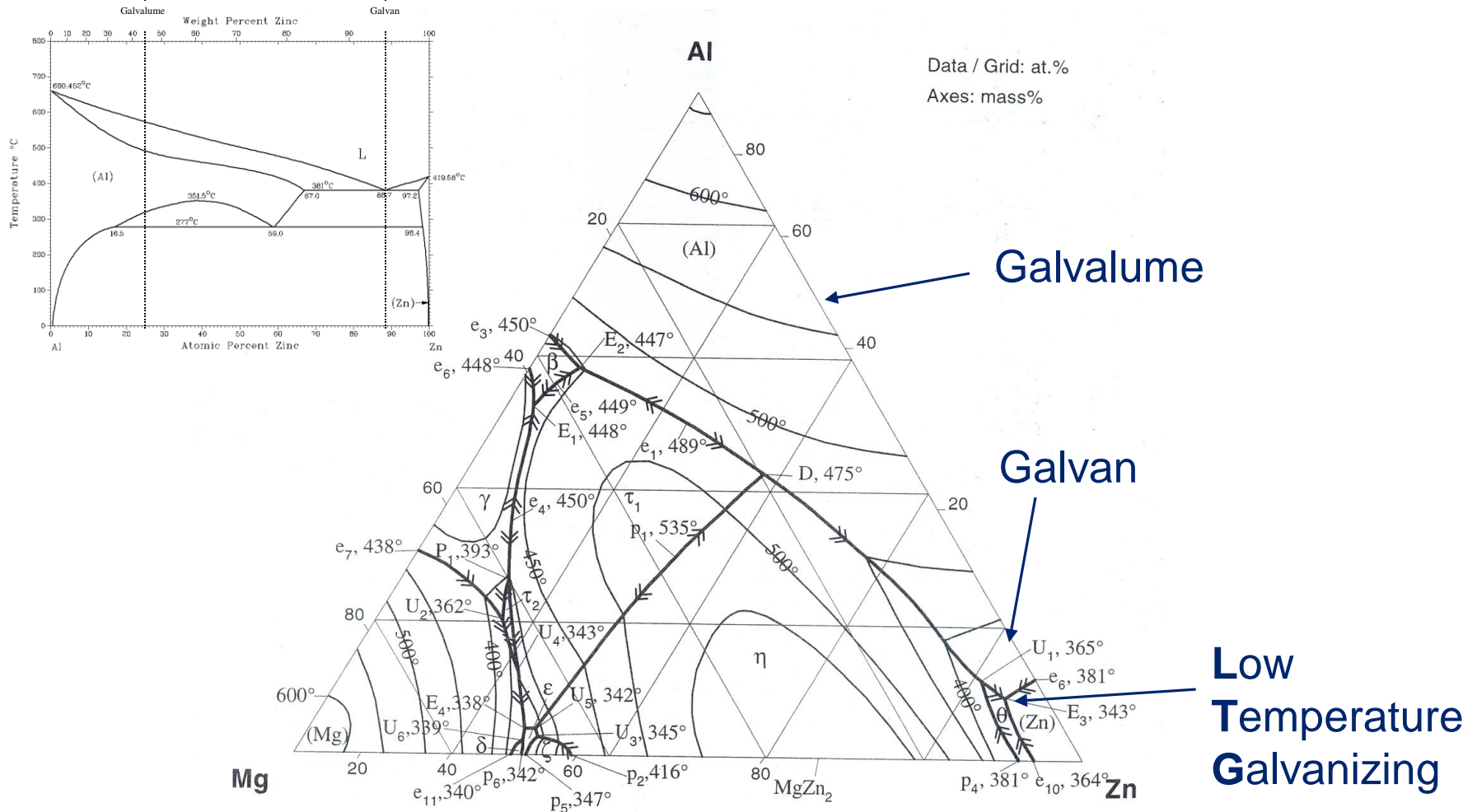
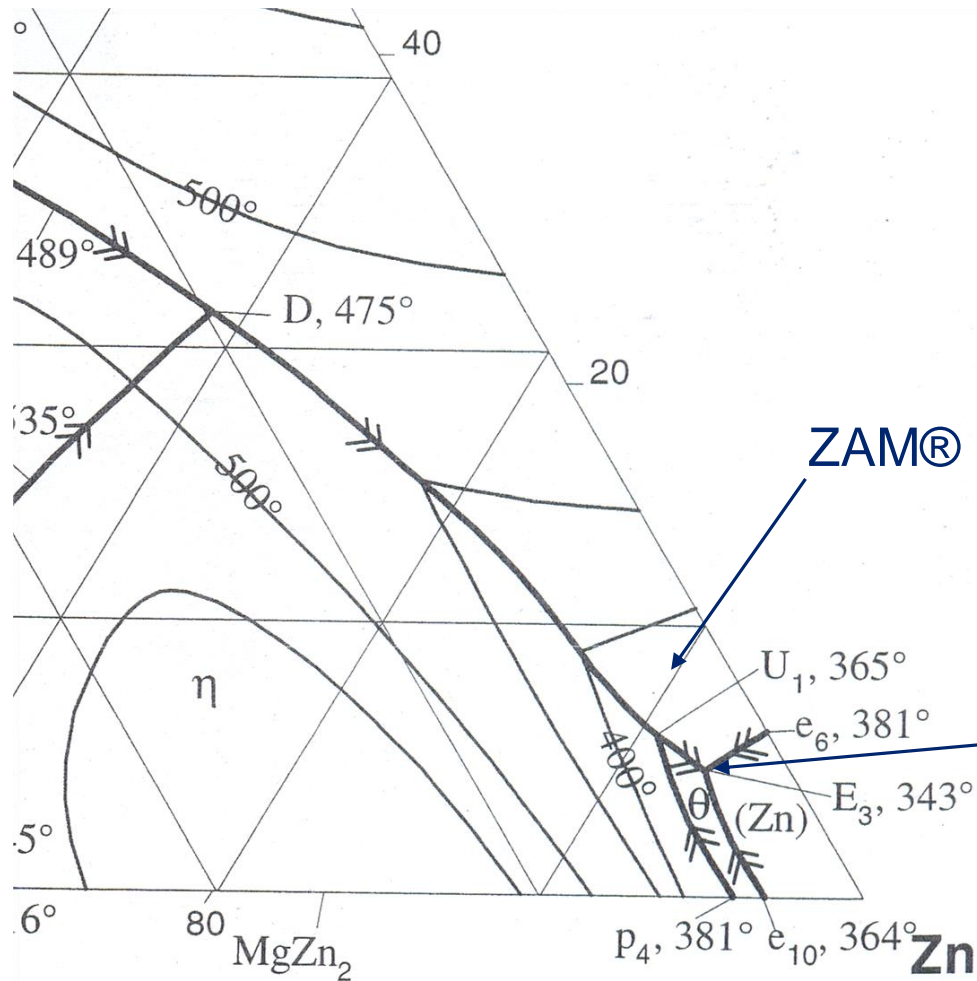


Figure 1: Liquidus surface



Alloy Development

Phase Diagram Zinc-Aluminium-Magnesium



Low Temperature Galvanizing

Alloy Development

Comparison ZAM / LTG

	ZAM® Existing alloy in Japan	LTG – new System
Composition of melting bath	91 % Zn 6 % Al 3 % Mg	92,95 % Zn 4,08 % Al 2,97 % Mg
Coating temperature	> 420 °C	< 400 °C
Application process	Continuous Coil Coating	Hot dip galvanizing of press hardened parts
Substrate material	Mild Steel	High and Ultra-High Strength Steels
Application	Structural parts for architecture and civil engineering	Structural parts for crash elements in automotive and BIW

Application process for new system

Substrate



Tin

Substrate



Zn-Al-Mg-Sn

Substrate

- Cleaning steel surface

- Pre-coating with tin
- Hot dip galvanizing process Zn-Al-Mg

- Diffusion of tin during hot dip galvanizing
- Change of ternary system in a quaternary system Zn-Al-Mg-Sn
- Influence to the melting process and phase creation



Corrosion Protection of High-Strength Steels

Characterization Microstructure

1

Corrosion Protection of Ultra-High Strength Steels

2

Alloy Development: Zn-Al-Mg System

3

Microstructure Characterization

4

Corrosion Performance

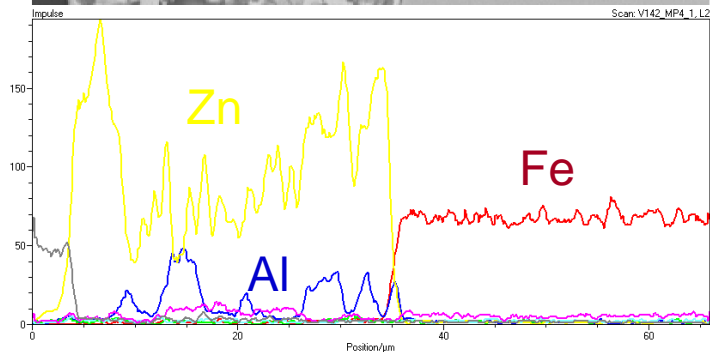
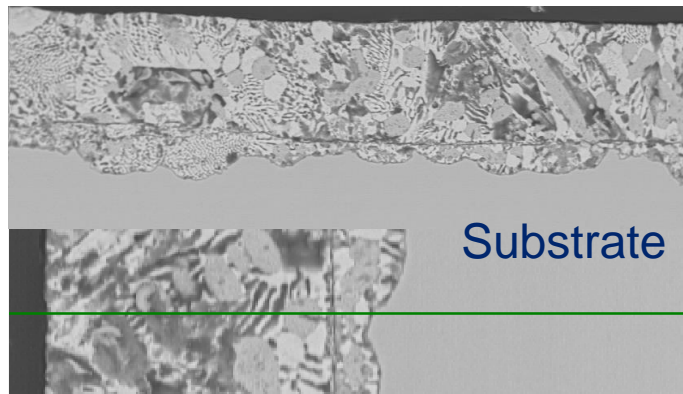
5

Summary

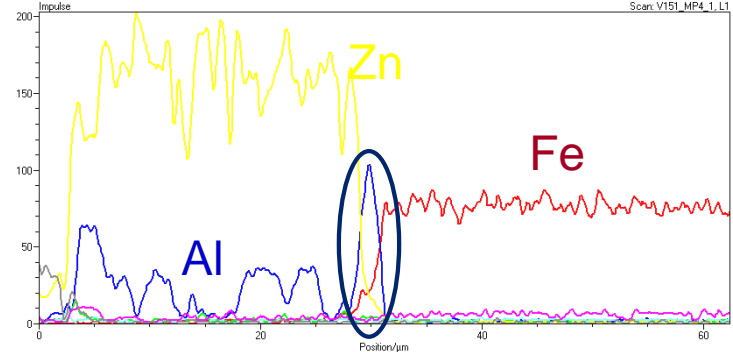
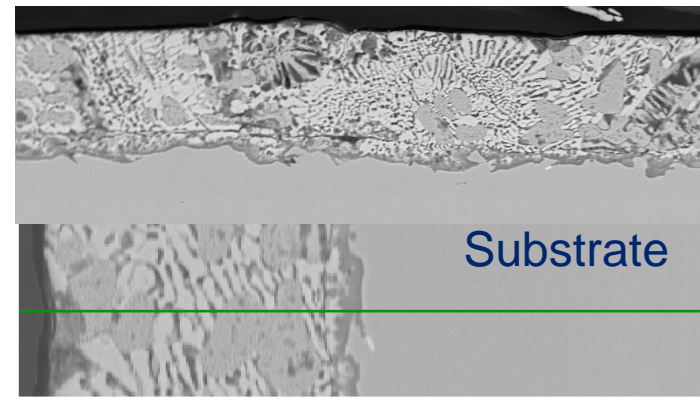
Microstructure Characterization

Influence of Exposure Time

9 min



20 min

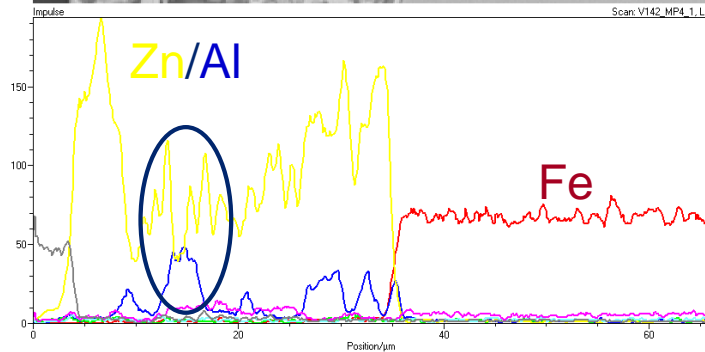
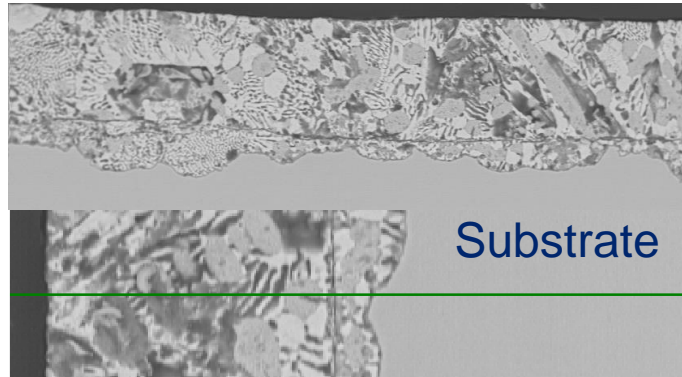


- Temperature 370 °C; ternary alloyed melting bath
- Ternary eutectic alloyed matrix
- Precipitations of Mg-Zn and Al-Zn
- Al is bonding layer between steel surface and coating
- Intermetallic compound of Fe-Al-Zn on the steel boundary layer

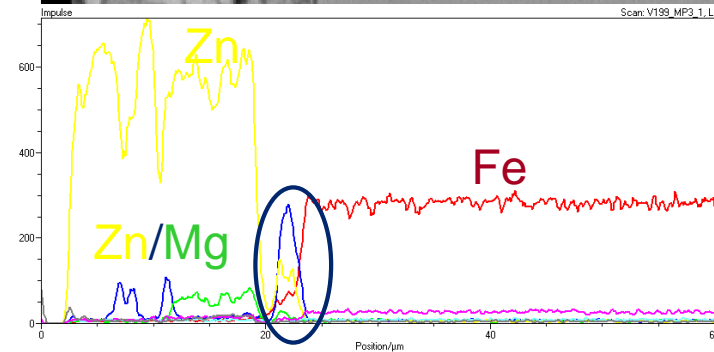
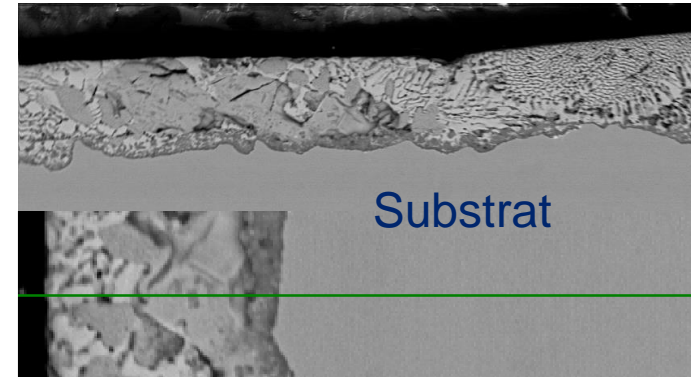
Microstructure Characterization

Influence of Temperature

370 °C, 9 min



390 °C, 9 min



- Ternary melting bath
- Different compounds of Mg-Zn-Al bzw. Al-Zn, MgZn₂
- Thickness of coating layer at 370 °C higher, ~35 μm
- Thickness of coating layer at 390 °C smaller, ~20 μm
- More intermetallic compounds on the steel surface as bonding layer

Corrosion Performance

1

Corrosion Protection of Ultra-High Strength Steels

2

Alloy Development: Zn-Al-Mg System

3

Microstructure Characterization

4

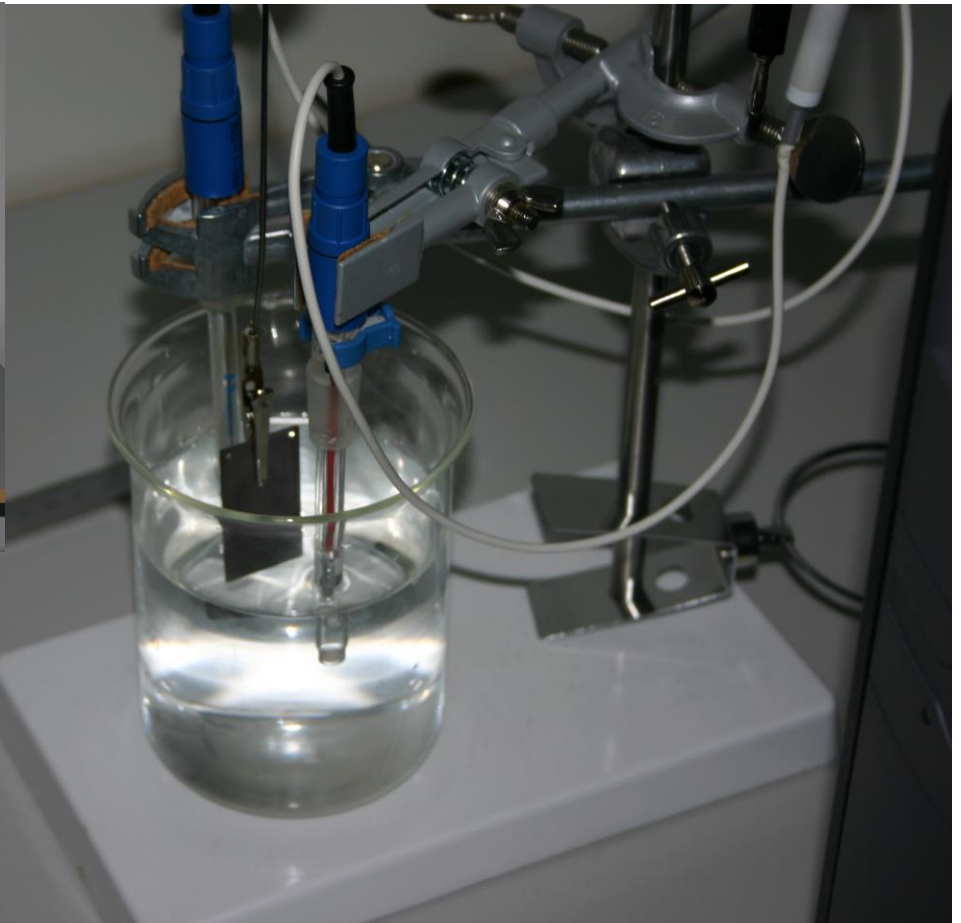
Corrosion Performance

5

Summary

Corrosion Performance

Corrosion Cell

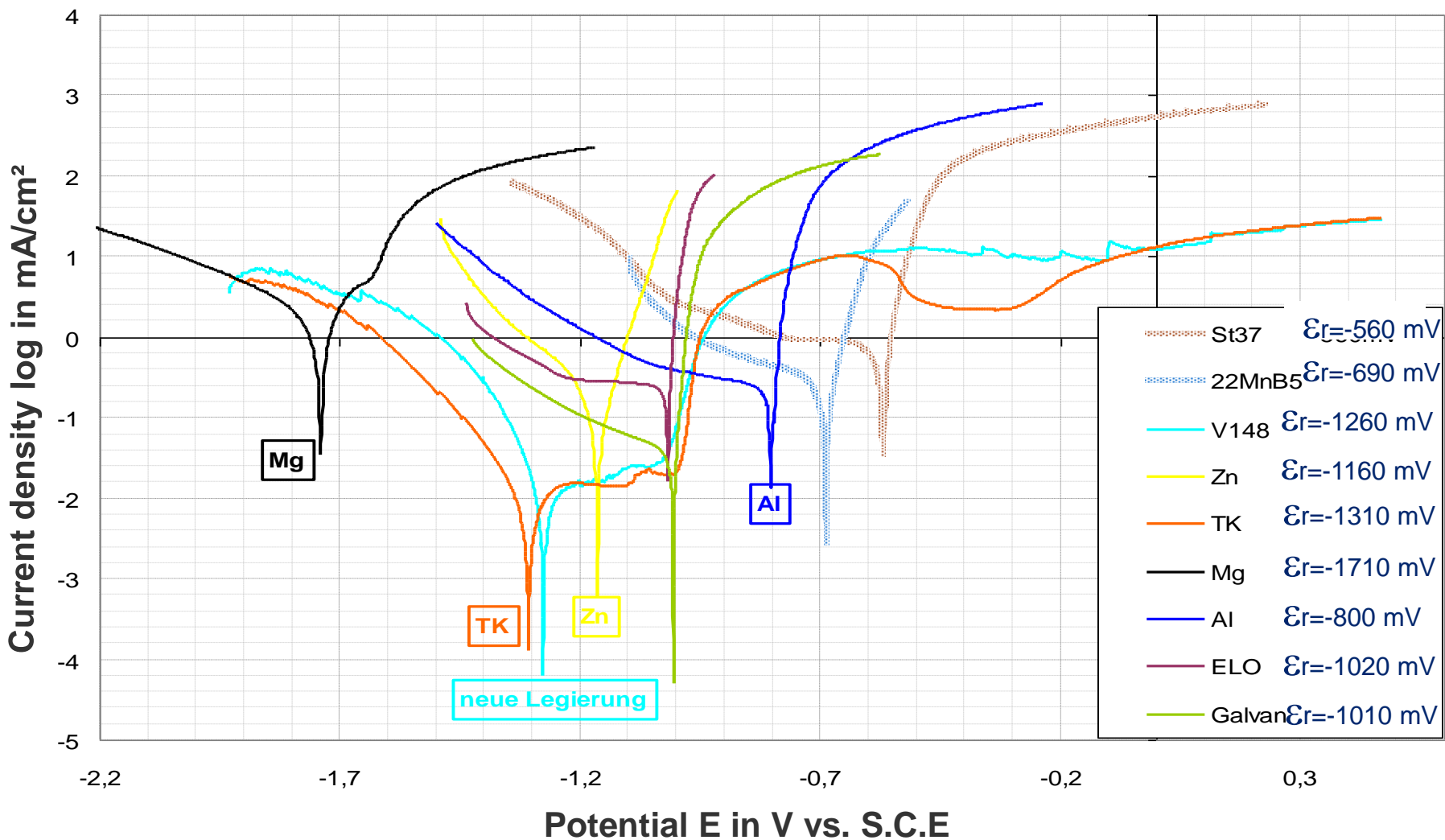


- Potentiostatic Polarisation Test
- Electrolyte: 3,5 % NaCl



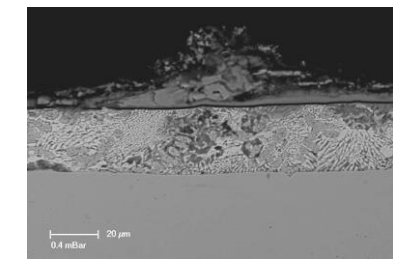
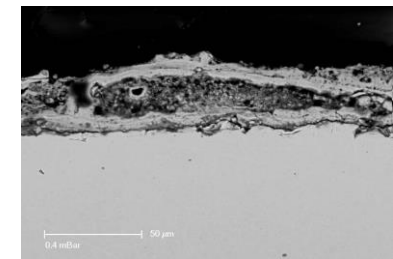
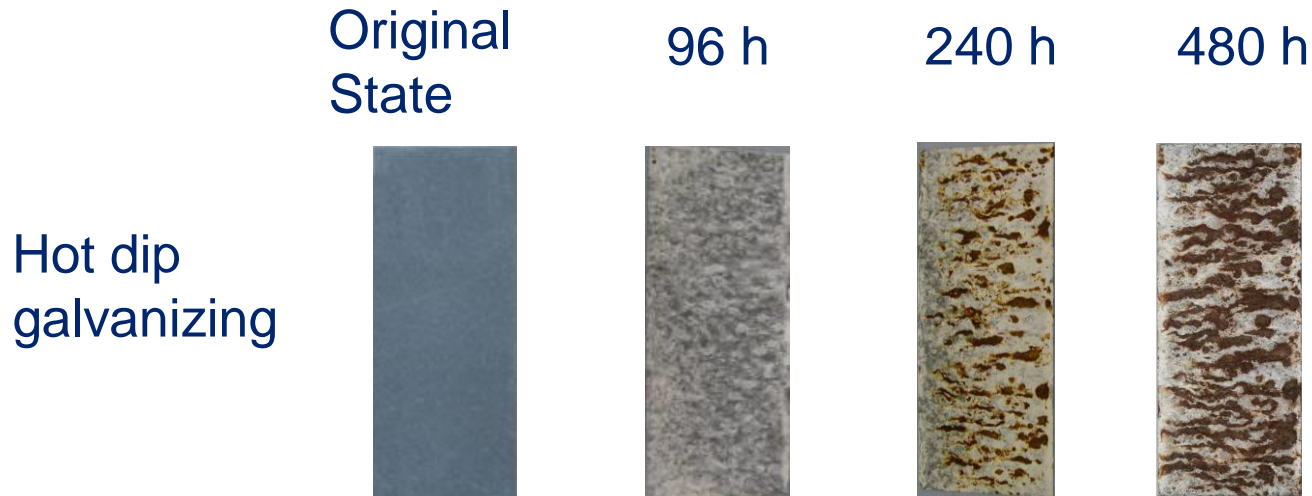
Corrosion Performance

Potentiostatic Polarisation Test



Corrosion Protection

DIN EN ISO 9227



5 % NaCl
Temperature 35 °C



Corrosion Protection of High-Strength Steels

Summary

1

Corrosion Protection of Ultra-High Strength Steels

2

Alloy Development: Zn-Al-Mg System

3

Microstructure Characterization

4

Corrosion Performance

5

Summary

Summary

- Low coating thickness possible – depends on temperature (10 to 40 μm)
- Influence of temperature to the coating microstructure and phases
- Less influence of exposure time to the coating microstructure
- Low Temperature Galvanizing – Coating layer ignoble compared to Zinc
- Cathodic corrosion protection for Al and steel substrate
- Good compatibility of coating with other coatings like Zn or Mg compounds
- Process without acid cleaning \Rightarrow no H_2 -embrittlement
- Tin detectible only on single areas or phase boundary
- No bad influence of tin for the corrosion protection
- Higher corrosion resistance of the new alloy



Thank you for your Attention

Contact:

Phone: +49 (0)8271-83-3522

E-Mail: verena.merklinger@sglcarbon.de